# Study of Free Vibration Analysis of Rectangular Laminated Plate With Circular Cut-Out

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Abstract- Composite materials are made from the combination of two or more materials with different chemical and physical properties, which when combined give a new material with enhanced material properties. Our study is concerned with the analysis of free vibration of rectangular plate with circular cut-out. We study the effects of aspect/size ratio, thickness ratio, and angle of the laminate, number of laminates, material properties and different boundary conditions.

Keywords- FEM, Composite materials, FSDT

## I. INTRODUCTION

A composite material is defined as a material which is composed of two or more materials at a microscopic scale and chemically distinct face. So, a composite material is heterogeneous at a microscopic scale but statistically homogeneous at macroscopic scale. The materials which form the composite are also called as constituents or constituent materials. The constituent materials of a composite have significantly different properties. Further, it should be noted that the properties of the composite formed may not be obtained from these constituents. However, a combination of two or more materials with significant properties will not suffice to be called as a composite material. Composite material are mainly used in sstructural, construction, medical, house-hold, industrial, transportation, electrical; electronics, etc. Metals are the most commonly used materials in these applications.

## **II. LITERATURE REVIEW**

S. Liu [1] studied a vibration analysis of composite laminated plates. D. Ngo-Cong et al [2] studied the free vibration analysis of laminated plates based on FSDT using one- dimensional IRBFN method.. Mohamed-Ouejdi Belarbi et al [3] uses a layer wise finite element formulation on the free vibration analysis of laminated composite and sandwich plates. T. Kant and K. Swaminathan [4] present the analytical solutions for free vibration of laminated composite and sandwich plates based on a higher order refined theory.

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Avadesh Kumar Sharma and N. D. Mittal [5] studied the free vibration analysis of laminated composite plates with elastically restrained edges using FEM. Harsh Kumar Bhardwaj et al [6] studied the free vibration analysis of laminated composite plates with skew cutouts based on FSDT. Pushpendra Kumar Sharma and Jyoti Vimal [7] studied the vibration analysis of laminated composite plates using FEM.

# **III. MATERIAL PROPERTIES**

Shell 181 elements is used for the analytical analysis of rectangular plate with circular hole. Following material properties are considered in the analysis:

$$E_{11}/E_{22}=25$$
,  $v_{12}=0.25$ ,  $G_{12}=G_{13}=0.5E_{22}$ ,  $G_{23}=0.2E_{22}$ 



Fig. Geometry of SHELL 181

Non-dimensional frequency is given by

$$\overline{\omega} = \frac{\omega b^2}{h} \sqrt{\frac{\rho}{E_{22}}}$$

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#### **IV. RESULT AND DISCUSSION**

Table1. Convergence study of non-dimensional frequencies for a cross-ply laminate, (a/b=1, h/b=0.01) for CCFF boundary condition for different mesh size  $(M \times N)$ 

				NIQUE				
	1	2	3	4	5	6	7	8
M=N								
7	5.4113	10.9971	25.7563	30.8719	34.1487	43.9286	49.1970	63.4234
Sharma	5.4691	11.1076	25.9892	31.3080	34.6154	44.4667	49.5819	64.0844
et al [7]								
9	5.4111	10.9930	25.6902	30.8605	34.1208	43.7862	48.7458	62.7503
Sharma	5.4686	11.1034	25.9228	31.2964	34.5858	44.4667	49.5819	64.0844
et al [7]								
11	5.4111	10.9909	25.6696	30.8574	34.1136	43.7541	48.5982	62.5748
Sharma	54686	11.1018	25.9017	31.2933	34.5790	44.2849	48.9807	63.2036
et al [7]								
13	5.4110	10.9909	25.6613	30.8553	34.1115	43.7428	48.5393	62.5108
Sharma	5.4686	11.1018	25.8932	31.2917	34.5763	44.2736	48.9211	63.1403
et al [7]								
15	5.4110	10.9909	25.6572	30.8553	34.1105	43.7387	48.5114	62.4829
Sharma	5.4686	11.1012	25.8895	31.2912	34.5753	44.2689	48.8931	63.1140
et al [7]								
17	5.4110	10.9909	25.6551	30.8553	34.1105	43.7356	48.4970	62.4695
Sharma	5.4686	11.1012	25.8874	31.2906	34.5748	44.2668	48.8789	63.0981
et al [7]								
19	5.4110	10.9909	25.6541	30.8543	34.1105	43.7345	48.4887	62.4612
Sharma	5.4686	11.1012	25.8864	31.2906	34.5748	44.2657	48.8710	63.0876
et al [7]								

# a) Rectangular Plates with Circular Hole

Table2. Variation of first ten natural frequencies with size ratio (a/b=1.5, 2, 2.5, 3) for a cross-ply laminate having circular cut-out at the centre,(r/b=0.1, h/b=0.01) for fully clamped boundary condition

Mode			a/b	
	1.5	2	2.5	3
1	19.256	19.105	16.139	17.137
2	29.016	25.843	24.797	22.169
3	40.159	35.066	28.297	25.564
4	48.942	41.505	34.601	29.864
5	53.238	43.089	37.929	37.907
6	63.587	53.005	46.705	39.886
7	68.969	61.104	48.705	45.051
8	77.956	66.539	58.422	49.983
9	91.046	74.034	59.326	60.195
10	95.437	81.366	63.651	61.851

From table 2 it is clear that natural frequencies of a rectangular plate with circular cut-out at the centre decreases with size ratio of plate except for first mode.

Table3. Variation of first ten natural frequency parameters

 $\overline{\omega} = \frac{\omega b^2}{h} \sqrt{\frac{\rho}{E_{22}}}$  with angle of ply ( $\Theta = 30^\circ, 45^\circ, 60^\circ, 90^\circ$ ) for a = 1.5 with circular an angle-ply laminate having size ratio a/b = 1.5 with circular cut-out at the centre,(r/b=0.1, h/b=0.01) for fully clamped boundary condition

Mode			e	
	30	45	60	90
1	62.452	18.140	18.565	19.256
2	95.365	28.480	28.848	29.016
3	126.128	39.033	39.777	40.159
4	151.628	46.008	47.109	48.942
5	165.483	52.201	52.844	53.238
6	197.04	62.705	63.589	63.587
7	208.854	67.305	68.383	68.969
8	234.210	73.550	75.052	77.956
9	263.881	87845	89.420	91.046
10	272.688	93.603	94.537	95.437

As seen from table 3 natural frequencies for first 10 modes of a rectangular plate with circular cut-out at the centre has a non-uniform variation.

Table4. Variation of first ten natural frequencies with different boundary conditions (CCCC, SSSS, CSCS, CFCF) for a crossply laminate having size ratio a/b=1.5 with circular cut-out at

the centre, (r/b=0.1, h/b=0.01)

Mode				
	CCCC	SSSS	CSCS	CFCF
1	19.256	7.307	10.451	7.229
2	29.016	16.109	23.665	8.232
3	40.159	23.185	25.218	15.323
4	48.942	29.043	38.685	17.626
5	53.238	33.397	44.775	22.091
6	63.587	41.853	52.075	29.386
7	68.969	47.232	59.035	34.537
8	77.956	53.169	60.574	35.686
9	91.046	64.382	69.181	41.846
10	95.437	67.247	80414	46.727

As seen from table 4 the values of natural frequency is maximum for fully clamped condition and minimum for all sides simply supported conditions.

Table5. Variation of first ten natural frequencies with thickness ratio (h/b=0.01, 0.05, 0.1, 0.5) for a cross-ply laminate having size ratio a/b=1.5 with circular cut-out at the centre,(r/b=0.1) for fully clamped boundary condition

Mode			h/b	
	0.01	0.05	0.1	0.5
1	19.256	2.215	125.101	1.733
2	29.016	3.322	16.900	2.464
3	40.159	4.629	21.641	3.251
4	48.942	5.655	25.130	3.891
5	53.238	6.202	26.871	4.142
6	63.587	7.546	30.429	4.785
7	68.969	8.067	32.562	5.145
8	77.956	9.012	35935	5.713
9	91.046	10.748	39.548	6.371
10	95.437	11.421	40.340	6.469

Table 5 shows the variation of first 10 natural frequencies of rectangular plate with circular cut-out with thickness. Natural frequency first decreases with thickness and then increases and again decreases.

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Table6. Variation of first ten natural frequencies with material properties ( $E_{11}/E_{22}=10, 15, 20, 25$ ) for a cross-ply laminate

having size ratio a/b=1.5 with circular cut-out at the centre,(r/b=0.1, h/b=0.01) for fully clamped boundary

condition

Mode			E11/E22	
	10	15	20	25
1	14.090	16.128	12.644	19.256
2	21.831	24.744	27.060	29.016
3	30.924	34.648	37.629	40.159
4	36.023	41.172	45.353	48.942
5	39.220	44.712	49.271	53.238
6	48.438	54.710	59.974	63.587
7	51.968	58.631	64.159	68.969
8	58.266	65.923	72.343	77.956
9	68.434	77.401	84.735	91.046
10	70.655	80.312	88.404	95.437

As shown in table 6 natural frequencies of rectangular plate with circular cut-out for first 10 modes of vibration increases with material property.

Table7. Variation of first ten natural frequencies with no. of layers (n=3, 5, 7, 9) for a cross-ply laminate having size ratio a/b=1.5 with circular cut-out at the centre, (r/b=0.1, h/b=0.01)dition £.11. 41

for fully	clamped	boundary	conditio	0
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Mode			n	
	3	5	7	9
1	19.256	24.662	25.352	25.305
2	29.016	36.035	36.730	36.493
3	40.159	52.412	54.430	54.560
4	48.942	60.859	61.950	61.608
5	53.238	67.144	69.203	69.161
6	63.587	80.479	83.350	83.680
7	68.969	84.820	86.811	86.581
8	77.956	101.471	106.007	106.884
9	91.046	112.717	115.505	115.288
10	95.437	117.229	121.224	121.534

As seen from table 7 the natural frequencies for a rectangular plate with circular cut-out for first 10 modes increases with increase in number of laminates of the plate.

# **V. CONCLUSIONS**

Following conclusions derived from the analytical analysis of rectangular plate with circular cut-out:

- Natural frequencies for first 10 modes of vibration for a rectangular plate with circular cut-out increases with angle of ply.
- Natural frequencies for first 10 modes of vibration for a rectangular plate with circular cut-out increases with material properties of plate.

- Natural frequencies for first 10 modes of vibration for a rectangular plate with circular cut-out increases with number of laminate in the plate.
- Natural frequencies for first 10 modes of vibration • for a rectangular plate with circular cut-out decreases with aspect/ size ratio.
- Natural frequencies for first 10 modes of vibration for a rectangular plate with circular cut-out increases with thickness ratio of the plate.
- Natural frequencies for first 10 modes of vibration for a rectangular plate with circular cut-out are maximum for fully clamped condition and minimum for all sides simply supported condition.

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