

Design of Integrated Double Buck–Boost Power Drive As High PF And Low THD Driver For Power-Led Lamps

Yallapu Raja Venkatesh¹, G.Raja Sekhar Yadav²

² Asst.Professor

^{1,2} Avanthi Engg College

Abstract- An integrated double buck-boost converter circuit, which can act as a high power factor, low output current ripple, and good efficiency driver for power LED lamps. The input stage is based on the integration of buck boost converter which performs power factor correction (PFC) from a universal ac source, using the PWM operation mode as a control loop. The integrated double buck-boost (IDBB) converter features one controlled switch and two inductors that supply a solid-state lamp from the mains, providing high power factor and good efficiency. In this project, the IDBB converter is analyzed with and without Control algorithm (PI controller), and a design methodology is proposed using Matlab. It is demonstrated that, with a careful design of the converter, the filter capacitances can be made small enough so that film capacitors may be used. The results obtained using PI controller and fuzzy logic controller for the same circuit are compared and are presented which validates high input power factor and superior control over the output voltage.

Keywords- IDBB Converter, PI Controller, THD Driver, LED Lamps, Matlab Tools.

I. INTRODUCTION

Energy prices have skyrocketed in recent years owing to depleting renewable resources. In addition to seeking other energy sources, countries worldwide are also initiating energy-saving and carbon reduction programs. Due to the small size and high efficiency, semiconductor lighting has attracted researchers and manufacturers to develop new products using this technology. Nowadays the energy-inefficient incandescent lamps and mercury-based tubular and compact fluorescent lamps are replacing LED lamps. Although HB white LEDs are not the most efficient lighting systems in terms of lumens per watt for streetlight applications (indeed, they achieve a lower efficiency than low-pressure sodium vapor lamps), they are quite interesting compared to traditional solutions due to their longer operating life and their more pleasant light spectrum (sodium lights emit only in yellow color, thus providing a very

poor Color Rendering Index, CRI). On the other hand global warming and increasing power demand etc. may be fulfilled by LEDs by implementing enhanced control technique (light dimming and preheating of filaments if possible). The high efficacy of power LEDs is only maintained under strict operating conditions, which include low direct current and low junction temperature (Fig 1).

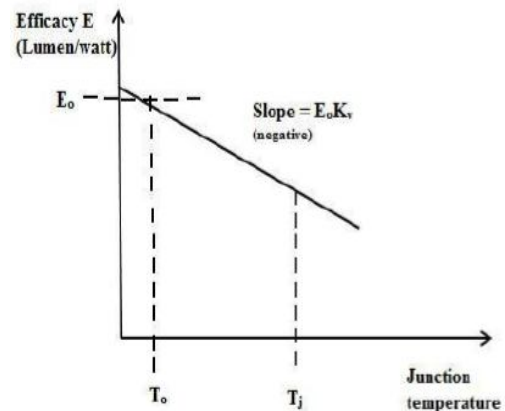


Figure 1: Efficiency versus junction temperature of LED

All these mean that the development of power supplies that achieve correct driving of the LED-based lamp is an important topic of research. White power LEDs are becoming an attractive light source, owing to their high reliability, long life, high color rendering index, and small size. In addition, there are commercially available units that can reach light efficacies as high as 100 lm/W. All these features make white LEDs a good candidate to override fluorescent and other discharge lamps. The main drawback of these LEDs is they need constant voltage as input and they need current limiter before the input of the LED.

This drive is currently implemented with power electronic stages based on switch mode power supplies (SMPS). However, an electrolytic capacitor is required in these applications. Unfortunately, the operating life of such capacitors is by far shorter than the life of the HB LEDs, and usually are the shortest of all the devices in the power supply.

Thus, removing the electrolytic capacitor would imply a remarkable increase in the operating life and reliability of the system. PFC converters can be classified into two types: two-stage and single-stage. Two-stage PFC converters consist of a PFC stage and a dc/dc stage. Single-stage PFC converters integrate the PFC stage and the dc/dc stage, leading to simple topology and low cost. They are suitable for low-power applications. The simplest active PFC circuits are implemented with a single-stage that makes the power factor correction.

II. IDBB CONVERTER

As explained in the introduction, the converter behaves as two buck–boost converters in cascade. The input buck–boost converter is made up by L_i , D_1 , CB , and M_1 , and the output buck–boost converter comprises L_o , D_2 , D_3 , C_o , and M_1 . The reversing polarity produced by the first converter in the capacitor CB is corrected by the second converter, given a positive output voltage with respect to ground. This simplifies the measurement of the load current for closed-loop operation, thus reducing sensing circuitry and cost. By operating the input inductor L_i in discontinuous conduction mode (DCM), the average current through the line will be proportional to the line voltage, therefore providing a near-unity PF. On the other hand, the output inductance L_o can be operated either in continuous conduction mode (CCM) or DCM. The operation in DCM has the advantage of providing a bus voltage across CB independent of the duty cycle and output power. However, it presents the disadvantage of requiring a higher value of the output capacitance to achieve low current ripple through the load.

In order to have a reduced value for the output capacitance, the output inductance is operated in CCM, because the current ripple is lower in this operation mode. In addition, the operation of the second stage in CCM with a duty cycle lower than 0.5 reduces the low-frequency ripple voltage since it is multiplied by the buck–boost converter voltage ratio. In this way, it will be possible to use a film capacitor to implement the output capacitance, thus having a higher life rating and better efficiency than using electrolytic capacitors.

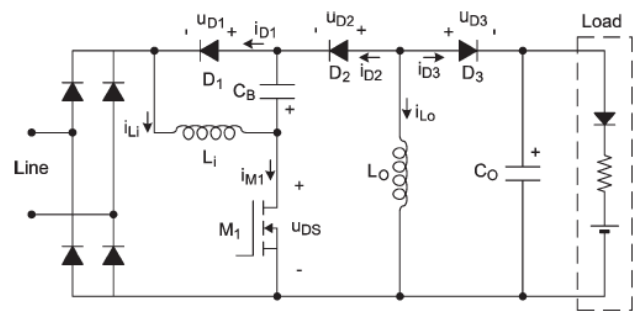


Figure 2: Schematic Diagram of the IDBB

III. ANALYSIS OF THE OFFLINE IDBB CONVERTER

In this section, the IDBB converter is analyzed when operated from the main voltage, achieving a near-unity input PF and a low-ripple current through the power-LED load. It is assumed that the line voltage is a sinusoidal waveform given as

$$v_g(t) = V_g \sin \omega t.$$

A. Line Current and Input Power

$$P_g = \frac{1}{2} V_g \langle i_g \rangle_{\text{peak}} = \frac{D^2 V_g^2}{4 L_i f_s}$$

B. Output and Bus Voltages

$$V_B = \frac{1-D}{D} V_o = \frac{(1-D)V_g}{2\sqrt{K}}, \quad V_B + V_o = \frac{V_g}{2\sqrt{K}}.$$

C. Reactive Components

$$L_o = \frac{D V_B}{0.5 \Delta I_{L_o_HF} f_s}$$

$$C_o = \frac{D I_o}{\Delta V_{O_HF} f_s}$$

Power Factor Requirements For Offline Led Drivers

- IEC (EU) requirements dictate THD performance for Lighting (over 25 W), other international standards apply depending on the region.
- US DOE ENERGY STAR includes mandatory PFC for Solid State Lighting regardless of the power level. This is a voluntary standard and applies to a specific set of products such as down

Lights, under cabinet Lights & desk lamps for example

- 1) >0.7 for residential applications
- 2) >0.9 for commercial applications
- While not absolutely mandated in the for lighting in all countries, it may be required based on the application:
- Utilities drive major commercial uses to have high PF at the facility level
- Moreover when utilities owns/service the streetlight it is in their interest to have good power factor, typically > 0.95+

IV. EXPERIMENTAL ANALYSIS

For the design of circuit component values, certain parameters are assumed approximately. Simulation results of IDBB converter using PI controller gives waveforms very close to standard waveforms. The input power factor of the converter can be viewed on the power factor display block. The control block as shown in figure generates the gate signal for controlling the switch .The rated current of the LED lamp which is 350 mA is given as current reference. The output current is subtracted from the reference current value to produce the error signal. This error signal is the input to the PI controller. The controller output is so as to maintain the output current value close to reference value. The output of PI controller is fed to the saturation block. The saturation block is used to limit the controller output to a limited range; the range being decided by the upper and lower limits of ramp signal, a pulse is generated. In simulation the output values for ramp signal are chosen as 0 and 1. Therefore the saturation upper and lower limits are taken as 0.9 & 0.1 respectively. The ramp signal and controller output signal are compared in the relational operator block. Whenever the Controller output is greater than the ramp signal, a pulse is generated.

Algorithm For Input Voltage To The IDBB Converter

- Step 1: start
- Step 2: Enter the voltage values ranging from 190 to 250 V.
- Step 3: Evaluate Source Voltage $V_s = V_{si}$
- Step 4: Measured lamp current, PF, THD, Efficiency as a function of the input voltage at closed loop operation

- Step 5: The above values (current, PF, THD, Efficiency) are noted for Buck Boost converter 1.
- Step 6: The Same procedure is implemented for Buck Boost converter 2.
- Step 7: Stop

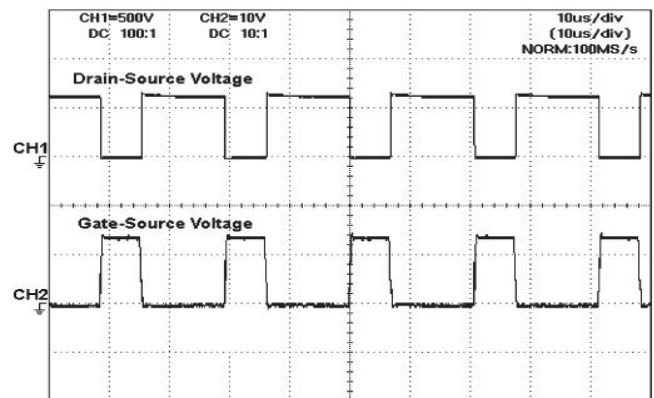


Figure 3: Waveforms in transistor M1 at 230-Vrms line voltage

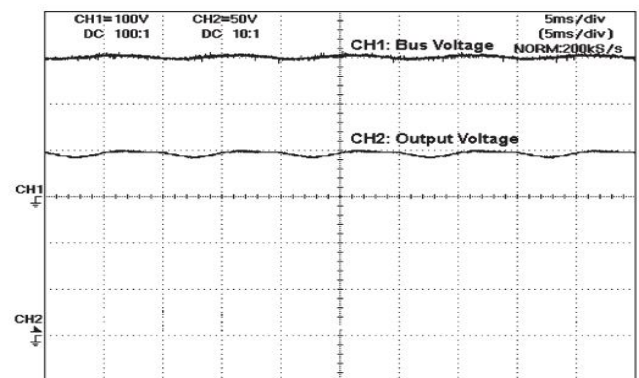


Figure 4: Bus and output voltages at nominal power and 230-Vrms line voltage.

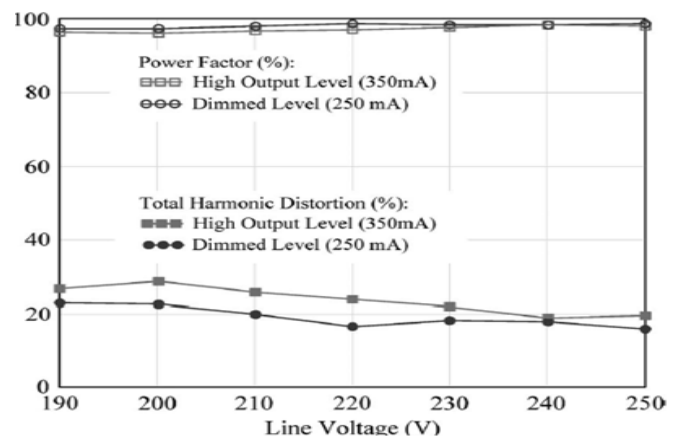


Figure 5: Measured PF and THD of the input current as a function of the line voltage.

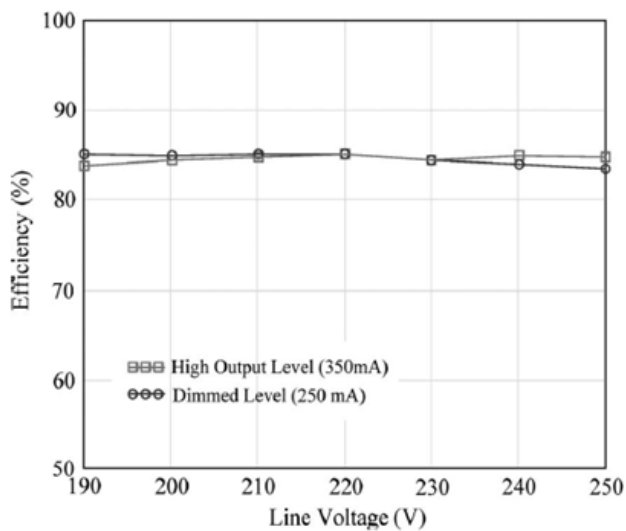


Figure 6: Measured converter efficiency as a function of the input voltage.

V. SIMULATION RESULTS

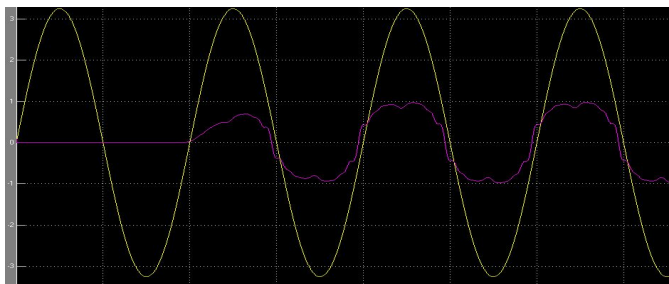


Figure 7: Line Voltage And Current At Nominal Power And 230-Vrms Line Voltage W.R.T Time (X & Y Axis)

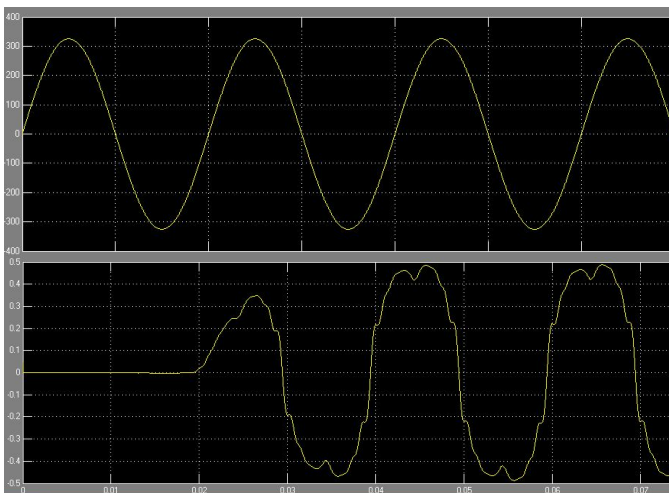


Figure 8: Input Voltage And Lamp Current W.R.T Time (X & Y Axis)

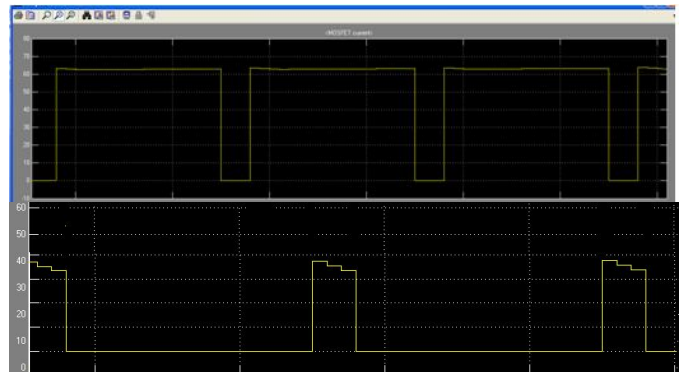


Figure 9: Input Pulses To Mosfet Switch W.R.T Time (X & Y Axis)

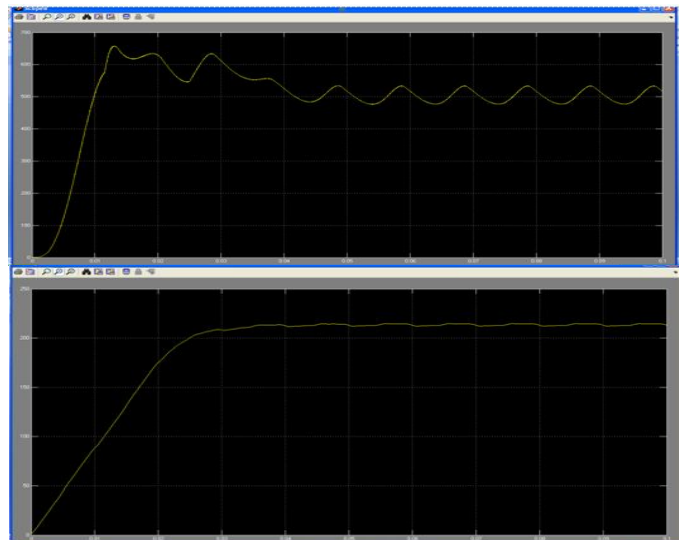


Figure 10: Output Voltage With & Without Pi Controller W.R.T Time (X & Y Axis)

VI. CONCLUSION & FUTURE SCOPE

An IDBB converter for power LED lamps was proposed which ensures high input power factor and low output ripple. The converter with PI control method was modeled in SIMULINK and waveforms were studied. The topology features two buck–boost converters in cascade but using only one controlled switch. By operating the input converter in DCM, a high input PF can be obtained. On the other hand, the operation of the second stage in CCM assures a low-ripple current through the LED load without using a very high output capacitance. In this way, the converter can be implemented using only film capacitors, avoiding the use of electrolytic capacitors and increasing the converter mean time between failures.

It can be used in led’s as the boost converter which boosts the energy and the led’s glow brightly. As now a days led’s are being used everywhere, this concept can be used for further better results. Even if any amount of rated voltage is

given the buck boost converter can handle it and send the required voltage to led's. It can be used even for the bunch of led's for maximum efficiency. The overall efficiency can be increased by using Fuzzy controller. Galvanic isolation can be provided in the circuit using an inductor in the output circuit. Automatic dimming controls can be implemented for better efficiency when used for street lighting applications.

converter,linProc.24thAnnu.IEEEAPec,feb.15–19,2009,pp.563–569. [13.]

REFERENCES

- [1] E. F. Schubert, *Light-Emitting Diodes*, 2nd ed. Cambridge, U.K.: Cambridge Univ. Press, 2006.
- [2] Cree XLamp XP-C LEDs, 2010, Data Sheet No. CLD-DS19 Rev 4.
- [3] Y. Fang, S.-H. Wong, and L. Hok-Sun Ling, "A power converter with pulse-level-modulation control for driving high brightness LEDs," in *Proc. 24th Annu. IEEE APEC*, Feb. 15–19, 2009, pp. 577–581.
- [4] R. A. Pinto, M. R. Cosetin, M. F. da Silva, G. W. Denardin, J. Fraytag, A. Campos, and R. N. do Prado, "Compact emergency lamp using power LEDs," in *Proc. 35th Annu. IEEE IECON*, Nov. 3–5, 2009, pp. 3494–3499.
- [5] D. R. Nuttall, R. Shuttleworth, and G. Routledge, "Design of a LED street lighting system," in *Proc. 4th IET Conf. PEMD*, Apr. 2–4, 2008, pp. 436–440.
- [6] H. Yuequan and M. M. Jovanovic, "A novel LED driver with adaptive drive voltage," in *Proc. 23rd Annu. IEEE APEC*, Feb. 24–28, 2008, pp. 565–571.
- [7] C. Qiao and K. M. Smedley, "A topology survey of single-stage power factor correction with a boost type inputcurrent-shaper," in *Proc. IEEE APEC 2000*, pp. 460–467.
- [8] H. Broeck, G. Sauerlander, and M. Wendt, "Power driver topologies and control schemes for LEDs," in *Proc. IEEE APEC 2007*, pp. 1319–1325.
- [9] J. Sebastian, D. G. Lamar, M. Arias, M. Rodriguez, and M. M. Hernando, "A very simple control strategy for power factor correctors driving high brightness light-emitting diodes," in *Proc. IEEE APEC 2008*, pp. 537–543.
- [10] W. Chang, D. Chen, H. Nien, and C. Chen, "A digital boost converter to drive white LEDs," in *Proc. IEEE APEC 2008*, pp. 558–564.
- [11] Z. Bo, Y. Xu, X. Ming, C. Qiaoliang, and W. Zhaoan, "Design of boost-flyback single-stage PFC converter for LED power supply without electrolytic capacitor for energy-storage," in *Proc. 6th IEEE IPEMC*, May 17–20, 2009, pp. 1668–1671.
- [12] K. I. Hwu, Y. T. Yau, and L.-L. Lee, "Powering LED using high-efficiency SR flyback